# Exam 2 <br> Chemical Reaction Engineering <br> 2 April 2001 <br> Closed Book and Notes 

( $\mathbf{3 0} \mathbf{~ p t s )}$ 1. You have been requested to troubleshoot problems with a well stirred reactor in your Texas chemical production plant. After taking the red eye flight and a long taxi ride to your hotel and then the plant your arrive exhausted, but eager to solve this problem. Apparently the problem with this 165 L reactor is that the conversion of the reactant, Anychemical, is too low at $X_{A}=0.53$. This reactor is heated using steam and you measure the temperature of the liquid inside the reactor at $130^{\circ} \mathrm{C}$. The initial concentration of Anychemical, A, is $10 \mathrm{~mol} \mathrm{~A} / \mathrm{L}$. The total flowrate of the liquid into the reactor is $5 \mathrm{~L} / \mathrm{min}$. You ask for reaction rate data, and are given the following table and graph from a 1 L batch reactor conducted at a temperature of $130^{\circ} \mathrm{C}$.

| t (min) | $\mathrm{CA}(\mathrm{mol} \mathrm{A} / \mathrm{L})$ |
| :---: | :---: |
| 0 | 10 |
| 1 | 9.4 |
| 5 | 8.1 |
| 10 | 6.4 |
| 15 | 5.3 |
| 20 | 4.7 |
| 25 | 3.7 |
| 30 | 3.25 |
| 35 | 2.8 |
| 40 | 2.4 |
| 45 | 2.3 |


a) In your eagerness to work on your first reactor troubleshooting problem, you have left your laptop with your luggage at the hotel. The best calculator that the plant can find is a basic ACME calculator without a regression program or any plotting features. After your initial disappointment, you realize that the reactor is a CSTR and you should be able to compare the measured values with the rate data provided by the lab (given above). Determine if there is a problem with this reactor.
b) Based on the above answer give a recommendation for improving the conversion of Anychemical.
( $\mathbf{3 0} \mathbf{~ p t s )}$ 2. The new products department has proposed a new chemical reaction to produce a chemical, Desiredchemical, D. This is a liquid phase reaction between Allchemical, A and Bestchemical, B. Unfortunately, undesired chemicals are also produced by this reaction, Undesiredone, U1, and Undesiredtoo, U2. The reaction scheme is given below:

$$
\begin{array}{ll}
A+B \xrightarrow{k_{1 A}} C+D & \text { where } r_{1 A}=-k_{1 A} C_{A} C_{B}[=] \frac{\mathrm{mol} A}{\mathrm{~m}^{3} \mathrm{~s}} \\
A+2 C \xrightarrow{k_{2 A}} U 1+U 2 & \text { where } r_{2 A}=-k_{2 A} C_{A} C_{C}^{2}[=] \frac{\mathrm{molA}}{\mathrm{~m}^{3} \mathrm{~s}}
\end{array}
$$

where $k_{1 A}=2.1 \times 10^{-3} \frac{\mathrm{~m}^{3}}{\mathrm{molB} \mathrm{s}} \exp \left(-\frac{3,300 \mathrm{~J} / \mathrm{mol}}{R T}\right)$
and $k_{2 A}=1.1 \times 10^{-5} \frac{\mathrm{~m}^{6}}{(\mathrm{molC})^{2} \mathrm{~s}} \exp \left(-\frac{5,200 \mathrm{~J} / \mathrm{mol}}{R T}\right)$
a) Suggests operating conditions of concentration and temperature for these proposed reactions that would maximize the selectivity, $S=\frac{r_{\text {Desired }}}{r_{\text {Undesired }}}$.
b) Suggest the best reactor scheme that would maximize the selectivity for this proposed reaction network. Draw a graph of the expected concentrations as a function of reactor volume.
c) Explain the next steps that you would take to optimize this reactor configuration.
(40 pts) 3. Maleic anhydride (MA, $\mathrm{C}_{4} \mathrm{H}_{2} \mathrm{O}_{3}$ ) was one of the products studied in a previous years reactor design project. One method to produce maleic anhydride is the partial oxidization of benzene $\left(\mathrm{B}, \mathrm{C}_{6} \mathrm{H}_{6}\right)$ with air. This gas phase reaction takes place in a tubular reactor with a solid vanadium pentoxide catalyst. Benzene enters the reactor at a molar flowrate of $26 \mathrm{~mol} / \mathrm{s}$ and air at $1,555 \mathrm{~mol} / \mathrm{s}$. The feed temperature for this reaction is 848 K and the pressure is at 5 atm . The following reactions are known to occur:
$\mathrm{C}_{6} \mathrm{H}_{6}+\frac{9}{2} \mathrm{O}_{2} \xrightarrow{k_{1}} \mathrm{C}_{4} \mathrm{H}_{2} \mathrm{O}_{3}+2 \mathrm{CO}_{2}+2 \mathrm{H}_{2} \mathrm{O}$
$\mathrm{C}_{4} \mathrm{H}_{2} \mathrm{O}_{3}+3 \mathrm{O}_{2} \xrightarrow{k_{2}} 4 \mathrm{CO}_{2}+\mathrm{H}_{2} \mathrm{O}$
$\mathrm{C}_{6} \mathrm{H}_{6}+\frac{15}{2} \mathrm{O}_{2} \xrightarrow{k_{3}} 6 \mathrm{CO}_{2}+3 \mathrm{H}_{2} \mathrm{O}$
The reaction rates are:
$r_{1}=-k_{1} C_{\mathrm{C}_{6} \mathrm{H}_{6}} C_{\mathrm{O}_{2}}$
$r_{2}=-k_{2} C_{\mathrm{C}_{4} \mathrm{H}_{2} \mathrm{O}_{3}} C_{\mathrm{O}_{2}}$
$r_{3}=-k_{3} C_{\mathrm{C}_{6} \mathrm{H}_{6}} C_{\mathrm{O}_{2}}$
with
$k_{1}=0.0637 \mathrm{~m}^{6} /\left(\mathrm{mol} \mathrm{O}_{2}\right.$ kgcat s $)$
$k_{2}=0.0664 \mathrm{~m}^{6} /\left(\mathrm{mol} \mathrm{O}_{2}\right.$ kgcat s$)$
$k_{3}=0.00348 \mathrm{~m}^{6} /\left(\mathrm{mol} \mathrm{O}_{2} \mathrm{kgcats}\right)$
Assuming that the tubular reactor contains 25 kg of catalyst and is isothermal and isobaric, construct a model of this reactor that will be used in a POLYMATH program. Your model should be able to predict the molar flowrate of each compound that enters or is produced in the reactor. Number each equation used in the POLYMATH program. Specify your initial conditions and final integration value.

Exam 2 Spring 2001 Solutions
$I \quad V=170.3 \mathrm{~L}$

$$
\begin{aligned}
& X_{A}=0.53 \\
& T=130^{\circ} \mathrm{C} \\
& C_{A_{0}}=\frac{10 \mathrm{~mol} \mathrm{~A}}{\mathrm{~L}} \\
& V_{0}=5 \mathrm{~L} / \mathrm{min}
\end{aligned}
$$



Mole balance

$$
\begin{aligned}
& 0=F_{A_{0}}-F_{A}+r_{A} V \\
& X_{A}=\frac{F_{A D}-F_{A}}{F_{A D}} \\
& 0=F_{A_{0}} X_{A}+r_{A} V \\
& \left.r_{A}=\frac{-F_{A_{D}} X_{A}}{V}=-\frac{(10 \mathrm{~mol} A}{\mathrm{K}}\right)(0.53) 5 \frac{\mathrm{~K}}{\min } \\
& 165 \mathrm{~L}
\end{aligned}-0.161 \frac{\mathrm{~mol} A}{L S}
$$

from graph at $X=0.53$

$$
\begin{aligned}
& \quad F_{A}=F_{A_{0}}(1-x)=\frac{10 \mathrm{~mol}}{L} \frac{5 L}{\min }(1-0.53)=23.5 \frac{\mathrm{~mol}}{\mathrm{~min}} \\
& C_{A}=\frac{F_{A}}{\nu}=\frac{23.5 \mathrm{~mol} / \mathrm{min}}{5 L / \mathrm{min}}=4.7 \mathrm{~mol} / \mathrm{L}
\end{aligned}
$$

USING GRAPH - the slope of the Curve at $C_{A}=4.7 \mathrm{~mol} / \mathrm{L}$ is

$$
\frac{d C_{A}}{d t}=\frac{7.7-0}{0-47.7}=-0.161 \mathrm{~mol} / \mathrm{L}
$$

Remember Batch $\frac{d C_{A} V}{d t}=r_{A} V$ constr $V \quad \frac{d C_{A}}{d t}=r_{A}$

Alternatively from rate data the expected conversion is :

$$
x_{A}=\frac{-r_{A V}}{F_{A_{0}}}=-\frac{(0.161 \mathrm{~mol} / \mathrm{min})(165 \mathrm{~L})}{10 \frac{\mathrm{~mol}}{\mathrm{~L}} \mathrm{AL}} \frac{5 \mathrm{Lin}}{\mathrm{~min}} \quad=0.53
$$

This reactor is working as expected
b) To increase conversion the reaction rate must be higher- see about increasing the reactor temperature.
2.

$$
\begin{aligned}
& A+B \rightarrow C+B \\
& A+2 C \rightarrow U_{1}+u 2 \\
& S=\frac{2.1 \times 10^{-3} e^{\left(-\frac{3300}{R T}\right) C_{A} C_{B}}}{2.1 \times 10^{-4}} \frac{\operatorname{exp(-\frac {5200}{RT})C_{A}C_{C}^{2}}}{} \\
& =10 \exp [1,900 / R T) \frac{C_{B}}{C_{C}^{2}}
\end{aligned}
$$

a) Conditions $T$ low
$C_{B}$ high
$C_{c}$ Low
b) Reactor operating conditions

tubular
 CA


This appears to be the best reactor since this reaction appears to be primarily a series type reaction. $-C_{D} \quad 1: 30$
C) Next steps


- construct a model and determine the appropriate volume for this reaction.

3. 

$$
\begin{aligned}
& F_{B_{0}}=26 \mathrm{~mol} / \mathrm{s} \quad \text { benzen } \\
& F_{A_{0}}=1,555 \mathrm{~mol} / \mathrm{s} \quad \text { ain } \\
& \left.T_{0}=848 \mathrm{k}\right)=T \\
& P_{0}=5 \mathrm{~atm}=P \\
& W=10 \mathrm{~kg}
\end{aligned}
$$

mole balances.

(2) $\frac{d F_{0}}{d \omega}=r_{0}$
(3) $\frac{d F_{m A}}{d w}=r_{m A}$
(4) $\frac{d f_{\mathrm{CO}_{2}}}{d w}=r_{\mathrm{CO}_{2}}$
(5) $\frac{d F_{w}}{d w}=r_{w}$
(6) $r_{B}=r_{1}+r_{3}$
( ) $r_{0}=r_{1} \frac{9}{2} \frac{\mathrm{molog}_{2}}{\mathrm{molB}}+\frac{3 \mathrm{molog}}{\mathrm{molmA}} r_{2}+\frac{15}{2} \frac{\mathrm{molog}}{\mathrm{molB}} \sqrt{3}^{2}$
(8) $r_{m A}=-r_{1}+r_{2}$
(a) $r_{\mathrm{CO}_{2}}=-\frac{2 \mathrm{mokO}_{2}}{\mathrm{molB}_{1}}-\frac{4 \mathrm{~mol} \mathrm{CO}_{2}}{\mathrm{molmA}} r_{2}-\frac{6 \mathrm{molCO}}{\mathrm{mol} B} r_{3}$
(10) $r_{w}=-\frac{2 \mathrm{molw}}{\mathrm{MOlB}} r_{1}-\frac{1 \mathrm{molw}}{1 \operatorname{molma}} r_{2}-\frac{3 \operatorname{mol} w}{1 \mathrm{molB}} r_{3}$
(11) $C_{B}=\frac{F_{B}}{2}$
(12) $C_{D}=\frac{F_{0}}{2}$
(13) $C_{M A}=\frac{F_{M A}}{2}$
(14) $F_{T}=F_{B}+F_{D}+F_{m A}+F_{{C O_{2}}+F_{W}+F_{N}, ~}^{\text {m }}$

$$
\frac{P \nu}{P_{0} \nu_{0}}=\frac{F_{T} R T}{F_{T_{0}} R T_{0}}
$$

(15) $\nu=\frac{F_{T}}{F_{T O}} \nu_{0}$
at $W=0 \quad F_{B}=26 \mathrm{~mol} / \mathrm{s}$

$$
\begin{aligned}
& F_{0}=0.21(1,555 \mathrm{~mol} / \mathrm{s})=326.55 \\
& F_{\text {mA }}=F_{\mathrm{CO}_{2}}=F_{W}=0
\end{aligned}
$$

(21) $F_{N}=0.79(1555 \mathrm{~mol} / \mathrm{s})$
(16) $r_{1}=-0.0637 \frac{\mathrm{~m}^{6}}{\text { mol } 0_{2} \text { kycats }} C_{B} C_{0}$
(17) $r_{2}=-0.0664 \frac{\mathrm{~m}^{6}}{\text { molo } 2 \mathrm{kgcat} \mathrm{s}} C_{\mathrm{mA}} C_{0}$
(18) $r_{3}=-0.00348 \frac{m^{6}}{\text { mol } O_{2} k_{g} \text { eat } s} C_{B} C_{0}$
stop at $w=10 \mathrm{~kg}$
12.5 min
(19) $\left.\nu_{0}=\frac{(1.555 \mathrm{~mol})}{\mathrm{s}}\right)\left(8.314 \frac{P_{a} \mathrm{~m}^{3}}{\mathrm{molk}}\right)(848 \mathrm{~K}) P \nu_{0}=f T_{0} R T_{0}$
(20) $F_{T_{0}}=26+1555$

## Exam 2:

## Homework for a maximum of 10 points added to exam score <br> Chemical Reaction Engineering <br> Due: Tuesday 10 April 2001 <br> OPEN Book and Notes

(30 pts) 1. You have been requested to troubleshoot problems with a well stirred reactor in your Texas chemical production plant. After taking the red eye flight and a long taxi ride to your hotel and then the plant your arrive exhausted, but eager to solve this problem. Apparently the problem with this 165 L reactor is that the conversion of the reactant, Anychemical, is too low at $X_{A}=0.53$. This reactor is heated using steam and you measure the temperature of the liquid inside the reactor at $130^{\circ} \mathrm{C}$. The initial concentration of Anychemical, A, is $10 \mathrm{~mol} \mathrm{~A} / \mathrm{L}$. The total flowrate of the liquid into the reactor is $5 \mathrm{~L} / \mathrm{min}$. You ask for reaction rate data, and are given the following table and graph from a 1 L batch reactor conducted at a temperature of $130^{\circ} \mathrm{C}$.

| $\mathrm{t}(\mathrm{min})$ | $\mathrm{CA}(\mathrm{mol} \mathrm{A} / \mathrm{L})$ |
| :---: | :---: |
| 0 | 10 |
| 1 | 9.4 |
| 5 | 8.1 |
| 10 | 6.4 |
| 15 | 5.3 |
| 20 | 4.7 |
| 25 | 3.7 |
| 30 | 3.25 |
| 35 | 2.8 |
| 40 | 2.4 |
| 45 | 2.3 |


a) In your eagerness to work on your first reactor troubleshooting problem, you have left your laptop with your luggage at the hotel. The best calculator that the plant can find is a basic ACME calculator without a regression program or any plotting features. After your initial disappointment, you realize that the reactor is a CSTR and you should be able to compare the measured values with the rate data provided by the lab (given above). Determine if there is a problem with this reactor.
b) Based on the above answer give a recommendation for improving the conversion of Anychemical.
c) Using either Excel or POLYMATH, determine the reaction rate constant and order for this reaction.
(30 pts) 2. The new products department has proposed a new chemical reaction to produce a chemical, Desiredchemical, D. This is a liquid phase reaction between Allchemical, A and Bestchemical, B. The desired production rate of D is $8 \mathrm{~mol} / \mathrm{s}$. You have feed concentrations of both A and B available in the range of 1 to $40 \mathrm{~mol} / \mathrm{L}$. Unfortunately, undesired chemicals are also produced by this reaction, Undesiredone, U1, and Undesiredtoo, U2. The reaction scheme is given below:

$$
\begin{array}{ll}
A+B \xrightarrow{k_{1 A}} C+D & \text { where } r_{1 A}=-k_{1 A} C_{A} C_{B}[=] \frac{\mathrm{mol} A}{L s} \\
A+2 C \xrightarrow{k_{2 A}} U 1+U 2 & \text { where } r_{2 A}=-k_{2 A} C_{A} C_{C}^{2}[=] \frac{\mathrm{mol} A}{L s}
\end{array}
$$

where $k_{1 A}=2.1 \frac{\mathrm{~L}}{\mathrm{~mol} \mathrm{~B} \mathrm{~s}} \exp \left(-\frac{6,200 \mathrm{~J} / \mathrm{mol}}{R T}\right)$
and $k_{2 A}=1.1 \frac{\mathrm{~L}^{2}}{(\mathrm{molC})^{2} \mathrm{~s}} \exp \left(-\frac{7,000 \mathrm{~J} / \mathrm{mol}}{R T}\right)$
a) Suggest general operating conditions of concentration and temperature for these proposed reactions that
would maximize the selectivity, $S=\frac{r_{\text {Desired }}}{r_{\text {Undesired }}}$. (e.g. high or low)
b) Suggest the best reactor scheme that would maximize the selectivity for this proposed reaction network.
c) Develop a POLYMATH model for a single PFR. Make a plot selectivity as a function of of the molar feed ratio of A to B . Make a second plot of temperature as a function of selectivity for a given feed ratio of $A$ to $B$.
d) Suggest a reactor volume, flowrate, and feed concentrations that you would recommend for this reaction to produce $8 \mathrm{~mol} / \mathrm{s}$ of D .
(40 pts) 3. Maleic anhydride (MA, $\mathrm{C}_{4} \mathrm{H}_{2} \mathrm{O}_{3}$ ) was one of the products studied in a previous years reactor design project. One method to produce maleic anhydride is the partial oxidization of benzene $\left(B, C_{6} \mathrm{H}_{6}\right)$ with air. This gas phase reaction takes place in a tubular reactor with a solid vanadium pentoxide catalyst. Benzene enters the reactor at a molar flowrate of $26 \mathrm{~mol} / \mathrm{s}$ and air at $1,555 \mathrm{~mol} / \mathrm{s}$. The feed temperature for this reaction is 848 K and the pressure is at 5 atm . The following reactions are known to occur:

$$
\begin{aligned}
& \mathrm{C}_{6} \mathrm{H}_{6}+\frac{9}{2} \mathrm{O}_{2} \xrightarrow{k_{1}} \mathrm{C}_{4} \mathrm{H}_{2} \mathrm{O}_{3}+2 \mathrm{CO}_{2}+2 \mathrm{H}_{2} \mathrm{O} \\
& \mathrm{C}_{4} \mathrm{H}_{2} \mathrm{O}_{3}+3 \mathrm{O}_{2} \xrightarrow{k_{2}} 4 \mathrm{CO}_{2}+\mathrm{H}_{2} \mathrm{O} \\
& \mathrm{C}_{6} \mathrm{H}_{6}+\frac{15}{2} \mathrm{O}_{2} \xrightarrow{k_{3}} 6 \mathrm{CO}_{2}+3 \mathrm{H}_{2} \mathrm{O}
\end{aligned}
$$

The reaction rates are:

$$
\begin{aligned}
& r_{1}=-k_{1} C_{\mathrm{C}_{6} \mathrm{H}_{6}} C_{\mathrm{O}_{2}} \\
& r_{2}=-k_{2} C_{\mathrm{C}_{4} \mathrm{H}_{2} \mathrm{O}_{3}} C_{\mathrm{O}_{2}} \\
& r_{3}=-k_{3} C_{\mathrm{C}_{6} \mathrm{H}_{6}} C_{\mathrm{O}_{2}}
\end{aligned}
$$

with
$k_{1}=0.0637 \mathrm{~m}^{6} /\left(\mathrm{molO}_{2}\right.$ kgcat s$)$
$k_{2}=0.0664 \mathrm{~m}^{6} /\left(\mathrm{molO}_{2} \mathrm{kgcat} \mathrm{s}\right)$
$k_{3}=0.00348 \mathrm{~m}^{6} /\left(\mathrm{mol} \mathrm{O}_{2}\right.$ kgcat s$)$
Assuming that the tubular reactor contains 25 kg of catalyst and is isothermal and isobaric, construct a model of this reactor that will be used in a POLYMATH program. Your model should be able to predict the molar flowrate of each compound that enters or is produced in the reactor. Number each equation used in the POLYMATH program. Specify your initial conditions and final integration value.

Exam 2: Problem 1
Rate Determination
t (min) CA (mol dC/dt A/L)

| 0 | 10 | 0.409 |
| ---: | ---: | ---: |
| 1 | 9.4 | 0.393 |
| 5 | 8.1 | 0.333 |
| 10 | 6.4 | 0.266 |
| 15 | 5.3 | 0.209 |
| 20 | 4.7 | 0.160 |
| 25 | 3.7 | 0.121 |
| 30 | 3.25 | 0.091 |
| 35 | 2.8 | 0.070 |
| 40 | 2.4 | 0.059 |
| 45 | 2.3 | 0.056 |



Reaction rate is:
$r_{A}=-0.0178\left(\frac{\mathrm{~L}}{\mathrm{~mol}}\right)^{0.4} \frac{1}{\min } C_{A}^{1.4}$

## POLYMATH Results

Exam 2 Problem 2Homework Solution- Selectivity in a PFR 04-03-2001, Rev5.1.224 Calculated values of the DEQ variables

| Variable | initial value | minimal value | maximal value | final value |
| :---: | :---: | :---: | :---: | :---: |
| V | 0 | 0 | 10 | 10 |
| FA | 10 | $1.364 \mathrm{E}-26$ | 10 | 1.364E-26 |
| FB | 40 | 30.634437 | 40 | 30.634437 |
| FC | 0 | 0 | 8.0966888 | 8.0966888 |
| FD | 0 | 0 | 9.3655629 | 9.3655629 |
| FU1 | 0 | 0 | 0.6344371 | 0.6344371 |
| FU2 | 0 | 0 | 0.6344371 | 0.6344371 |
| flow | 1 | 1 | 1 | 1 |
| CB | 40 | 30.634437 | 40 | 30.634437 |
| T | 300 | 300 | 300 | 300 |
| k1 | 0.1748495 | 0.1748495 | 0.1748495 | 0.1748495 |
| k2 | 0.0664569 | 0.0664569 | 0.0664569 | 0.0664569 |
| CC | 0 | 0 | 8.0966888 | 8.0966888 |
| CA | 10 | 1.364E-26 | 10 | $1.364 \mathrm{E}-26$ |
| r2 | 0 | -1.6811659 | 0 | -1.115E-26 |
| r1 | -69.939803 | -69.939803 | -7.306E-26 | -7.306E-26 |
| S | 0 | 0 | 4.8428526 | 3.2759328 |
| Soverall | 0 | 0 | 10.859248 | 7.3810022 |

## ODE Report (RKF45)

Differential equations as entered by the user
[1] $d(F A) / d(V)=r 1+r 2$
[2] $d(F B) / d(V)=r 1$
[3] $d(F C) / d(V)=-r 1+2^{*} r 2$
[4] $d(F D) / d(V)=-r 1$
[5] $\quad d(F U 1) / d(V)=-r 2$
[6] $d(F U 2) / d(V)=-r 2$
Explicit equations as entered by the user
[1] flow = 1
[2] $\mathrm{CB}=\mathrm{FB}$ /flow
[3] $\mathrm{T}=300$
[4] $\mathrm{k} 1=2.1^{*} \exp (-6200 / 8.314 / \mathrm{T})$
[5] k2 $=1.1^{*} \exp (-7000 / 8.314 / \mathrm{T})$
[6] CC = FC/flow
[7] CA = FA/flow
[8] $\mathrm{r} 2=-\mathrm{k} 2^{*} \mathrm{CA}{ }^{*} \mathrm{CC}^{\wedge 1} 1.2$
[9] $r 1=-k 1^{*} C A^{*} C B$
[10] $S=$ if $(r 2<0)$ then $(r 1 / r 2 / 2)$ else ( 0 )
[11] Soverall $=$ if $(F U 1>0)$ then (FD/(FU1+FU2)) else (0)
Independent variable
variable name : V
initial value : 0
final value : 10
Precision
Step size guess. $\mathrm{h}=0.000001$
Truncation error tolerance. $\mathrm{eps}=0.000001$
General
number of differential equations: 6
number of explicit equations: 11
Data file: G:ICourses 14 june 2000\Reaction
Engineering\Exams\&Quizzeslexam2problem2selectivity_hmwk.pol

## Problem 3

## POLYMATH Results

Exam 2 Multiple Rates Maleic Anhydride 04-02-2001, Rev5.1.224
Calculated values of the DEQ variables

| Variable | initial value | minimal value | maximal value | final value |
| :---: | :---: | :---: | :---: | :---: |
| W | 0 | 0 | 25 | 25 |
| FB | 26 | 6.2902951 | 26 | 6.2902951 |
| FO | 326.55 | 240.91275 | 326.55 | 240.91275 |
| FMA | 0 | 0 | 8.2091187 | 8.0513837 |
| FCO2 | 0 | 0 | 55.627586 | 55.627586 |
| FW | 0 | 0 | 35.865177 | 35.865177 |
| FT0 | 1581 | 1581 | 1581 | 1581 |
| FN | 1228.45 | 1228.45 | 1228.45 | 1228.45 |
| FT | 1581 | 1575.1972 | 1581 | 1575.1972 |
| flowrate0 | 22.001441 | 22.001441 | 22.001441 | 22.001441 |
| flowrate | 22.001441 | 21.920688 | 22.001441 | 21.920688 |
| CO | 14.84221 | 10.9902 | 14.84221 | 10.9902 |
| CMA | 0 | 0 | 0.3743857 | 0.3672961 |
| r2 | 0 | -0.2880872 | 0 | -0.2680341 |
| CB | 1.1817408 | 0.286957 | 1.1817408 | 0.286957 |
| r1 | -1.1172753 | -1.1172753 | -0.2008916 | -0.2008916 |
| r3 | -0.061038 | -0.061038 | -0.0109749 | -0.0109749 |
| rB | -1.1172753 | -1.1172753 | -0.4689257 | -0.4689257 |
| ro | -5.4855238 | -5.4855238 | -1.7904266 | -1.7904266 |
| rMA | 1.1172753 | -0.0671424 | 1.1172753 | -0.0671424 |
| rCO2 | 2.6007785 | 1.5397692 | 2.6596228 | 1.5397692 |
| rW | 2.4176646 | 0.7027421 | 2.4176646 | 0.7027421 |
| X | 0 | 0 | 0.7580656 | 0.7580656 |

## ODE Report (RKF45)

Differential equations as entered by the user
[1] $d(F B) / d(W)=r B$
[2] $\mathrm{d}(\mathrm{FO}) / \mathrm{d}(\mathrm{W})=\mathrm{rO}$
[3] $\mathrm{d}(\mathrm{FMA}) / \mathrm{d}(\mathrm{W})=\mathrm{rMA}$
[4] $\mathrm{d}(\mathrm{FCO} 2) / \mathrm{d}(\mathrm{W})=\mathrm{rCO} 2$
[5] $d(F W) / d(W)=r W$
Explicit equations as entered by the user
[1] $\mathrm{FTO}=26+1555$
[2] $\mathrm{FN}=0.79 * 1555$
[3] $\mathrm{FT}=\mathrm{FB}+\mathrm{FO}+\mathrm{FMA}+\mathrm{FCO} 2+\mathrm{FW}+\mathrm{FN}$
[4] flowrate0 $=$ FT0*8.314*848/5/1.01325e5
[5] flowrate $=$ FT/FT0*flowrate0
[6] CO = FO/flowrate
[7] CMA = FMA/flowrate
[8] $\mathrm{r} 2=-0.0664^{*} \mathrm{CMA} * \mathrm{CO}$
[9] $\mathrm{CB}=\mathrm{FB} /$ flowrate
[10] r1 $=-0.0637^{*} \mathrm{CB}^{*} \mathrm{CO}$
[11] $\mathrm{r} 3=-0.00348^{*} \mathrm{CB}{ }^{*} \mathrm{CO}$
[12] $\mathrm{rB}=\mathrm{r} 1+\mathrm{r} 2$
[13] $\mathrm{rO}=9 / 2^{*} \mathrm{r} 1+3^{*} \mathrm{r} 2+15 / 2^{*} \mathrm{r} 3$
[14] $\mathrm{rMA}=-\mathrm{r} 1+\mathrm{r} 2$
[15] $\mathrm{rCO} 2=-2^{*} \mathrm{r} 1-4^{*} \mathrm{r} 2-6^{*} \mathrm{r} 3$
[16] $\mathrm{rW}=-2^{*} \mathrm{r} 1-\mathrm{r} 2-3^{*} \mathrm{r} 3$
[17] $X=(26-F B) / 26$
Independent variable
variable name : W
initial value : 0
final value : 25

Precision
Step size guess. $\mathrm{h}=0.000001$
Truncation error tolerance. eps $=0.000001$
General
number of differential equations: 5
number of explicit equations: 17
Data file: G:ICourses 14 june 2000\Reaction Engineering\Exams\&Quizzes\maleicanhydride.pol

